



framatome

Performance of M5_{Framatome} cladding during Loss-of- Coolant Accident

Borrossi Romain, Chosson Raphaël, Haller
Xavier

Nessebar, Bulgaria & 14-19/09/2025

LOCA regulatory context

Historical requirements in 1970 s:

- Empirical limit based on ring compression tests and the Baker-Just (BJ) correlation for total oxidation
- $PCT < 1204\text{ }^{\circ}\text{C}$ and Equivalent Cladding Reacted (ECR) $< 17\%$

Experimental programs have shown the detrimental effect of hydrogen content on the post-oxidation mechanical behavior. Different H sources:

- In-service H pickup
- Breakaway oxidation phenomenon
- Secondary hydriding phenomenon

Limits changed to be dependent on H

- US NRC 10 CFR 50.46c, via draft regulatory guide DG-1263 (in discussion since circa 2010)
 - PCT and CP-ECR limit dependent on H
 - Experimental basis: post-quench ductility assessed by ring compression tests (RCT)
 - Additional focus on breakaway oxidation
- French GP Critère 2014 (A. Cabrera and N. Waeckel, 2015):
 - PCT remains $1204\text{ }^{\circ}\text{C}$ but BJ-ECR limit dependent on H
 - Experimental basis (similar to Japan's): semi-integral LOCA tests with axial loading during the final quench

Content

1. In-service
corrosion and H
pickup

2. High
temperature
oxidation behavior

3. Post-oxidation
mechanical
behavior

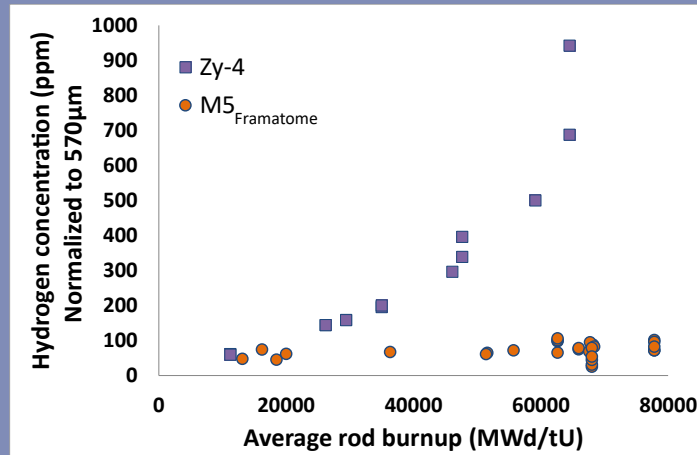
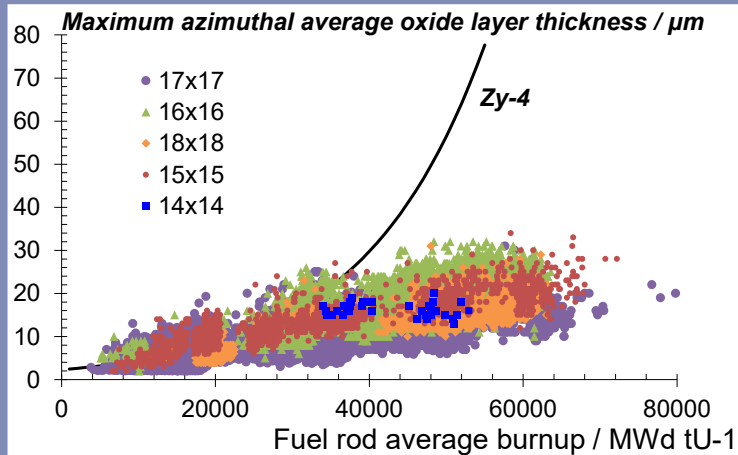
In-service corrosion and H uptake – PWR and VVER

M5_{Framatome}* cladding: fully recrystallized Zr-1%Nb-O alloy with controlled Fe and S content

Absence of Sn results in a very low corrosion rate and H pickup

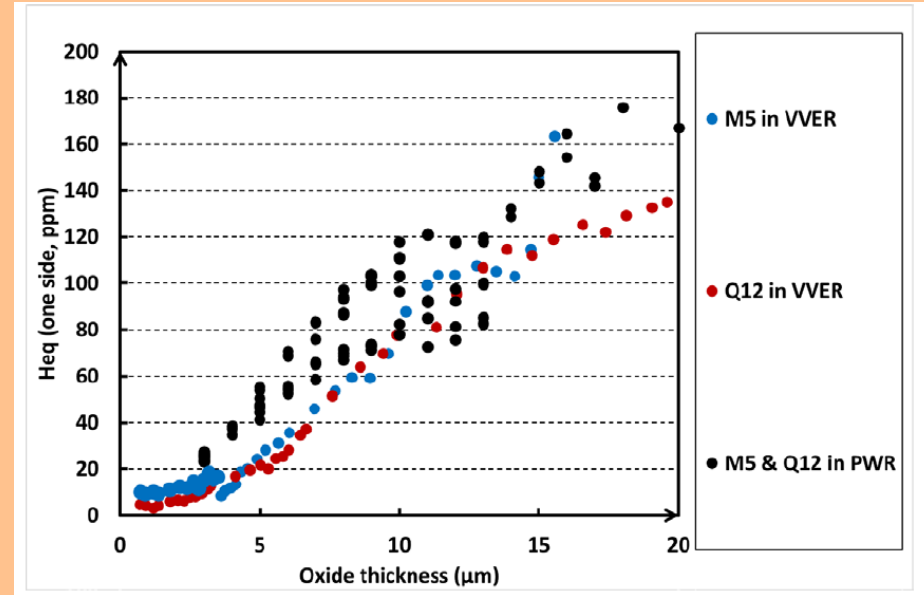
PWR OPEX:

- Slow corrosion kinetics compared to Zy-4
- End-of-life max. H content around 100 wppm



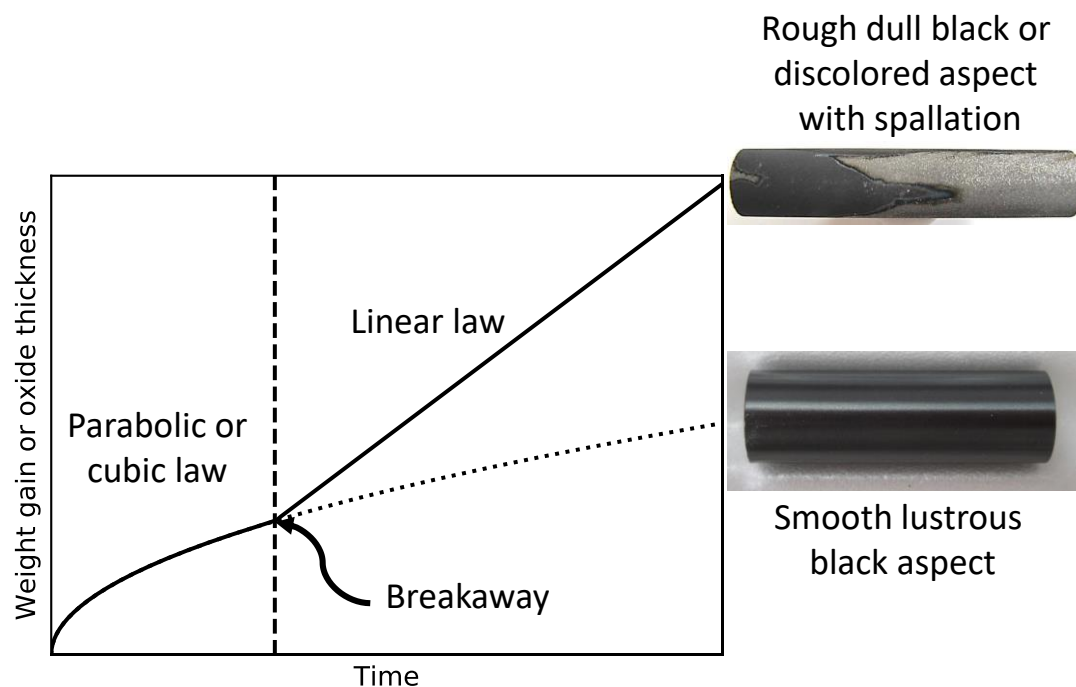
Autoclave testing:

Similar corrosion and H pickup rates between VVER1000 and PWR conditions



High-temperature oxidation phenomena

Oxidation kinetics



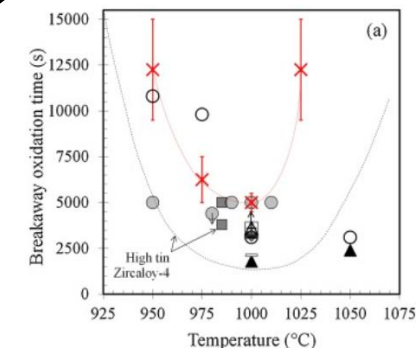
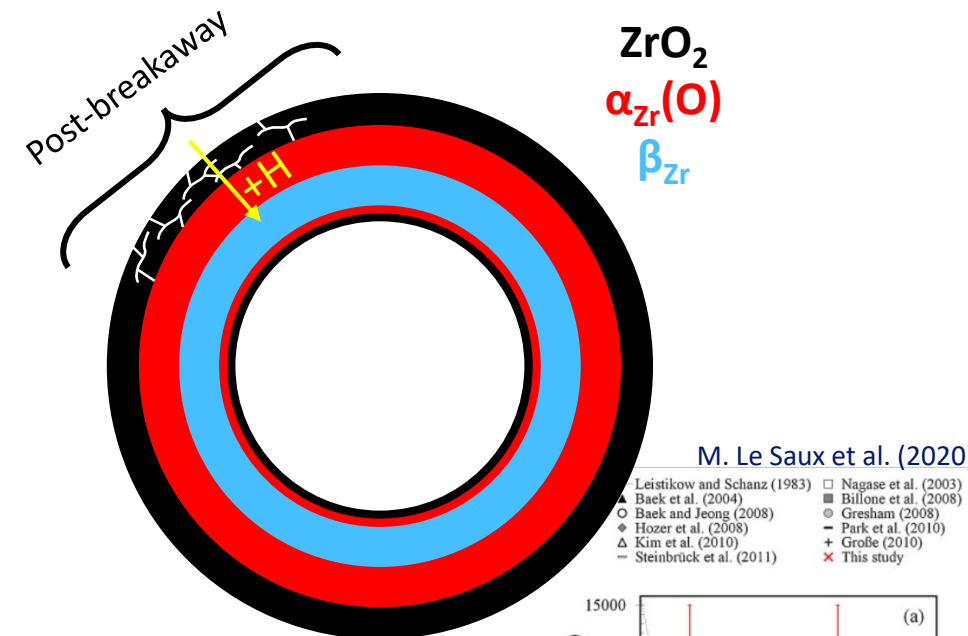
Breakaway:

H uptake in the range of hundreds of wppm

Onset time temperature dependent and affected by surface damage

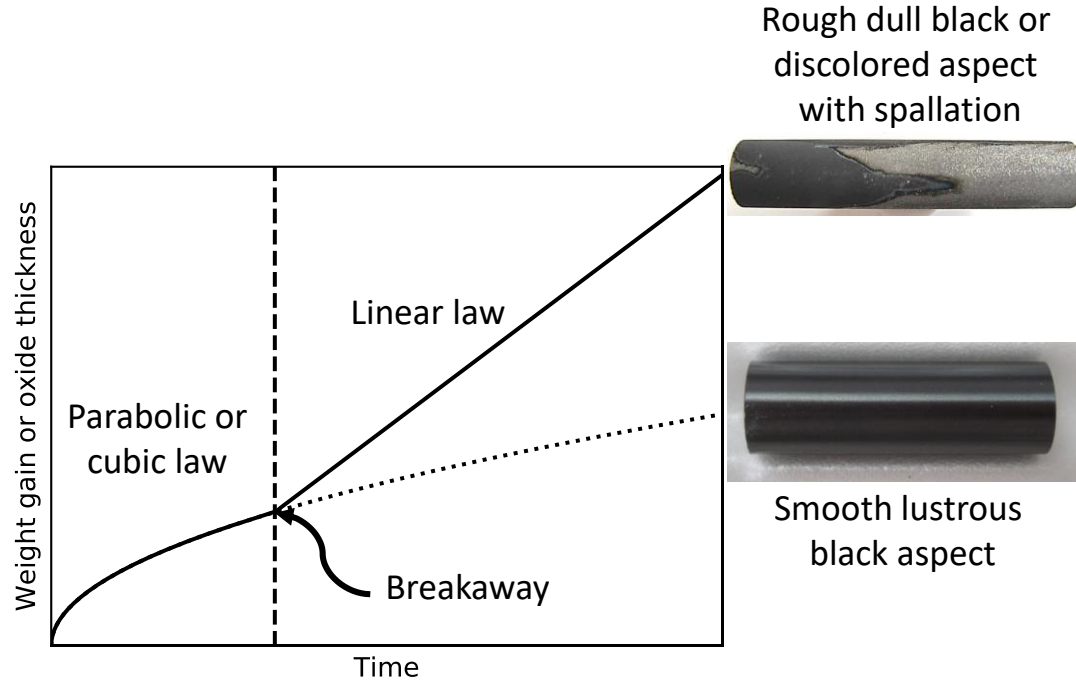
Shortest onset time typically occurs for $T \sim 1000^\circ\text{C}$

Cladding cross-section

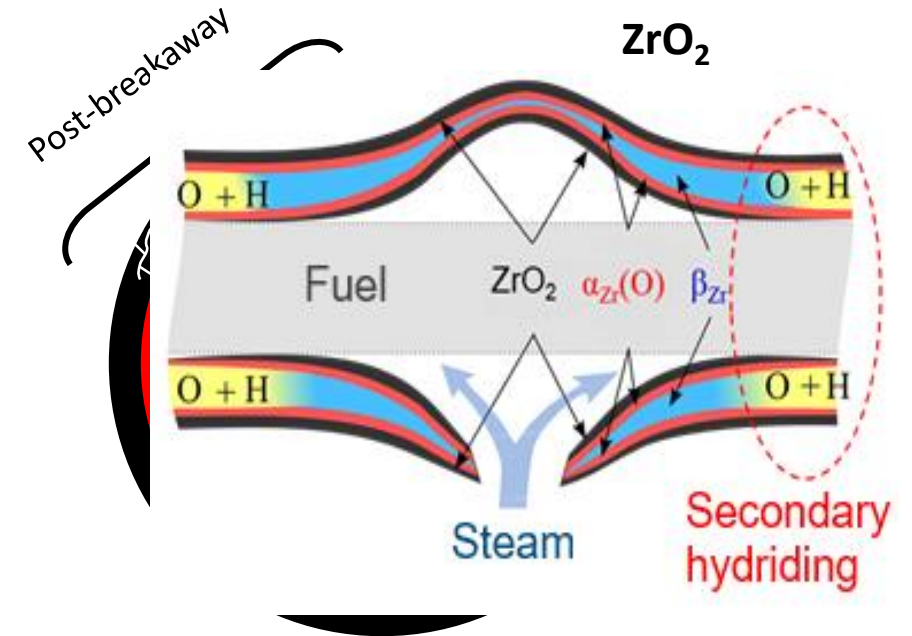


High-temperature oxidation phenomena

Oxidation kinetics



Cladding secondary hydriding



Breakaway:

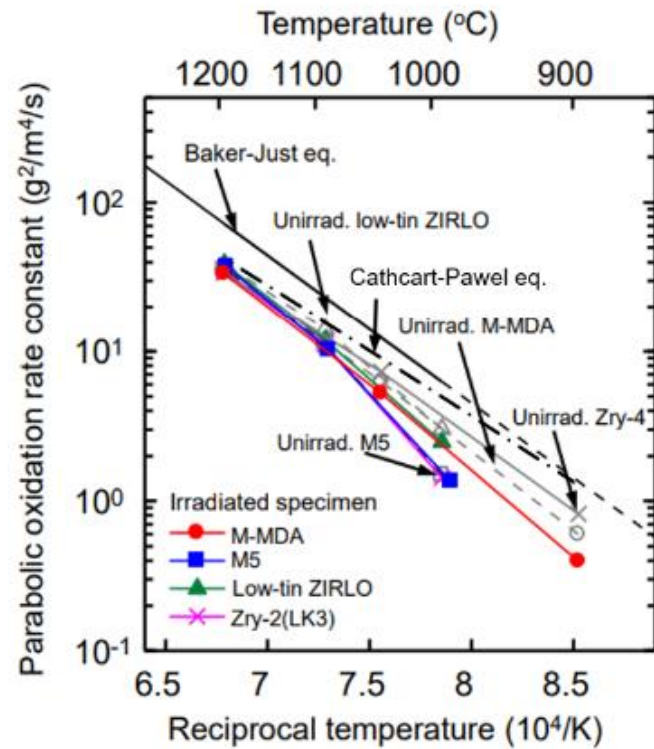
H uptake in the range of hundreds of wppm to 3000-4000 wppm a few millimeters

Onset time temperature dependent and affected by surface damage from the burst opening

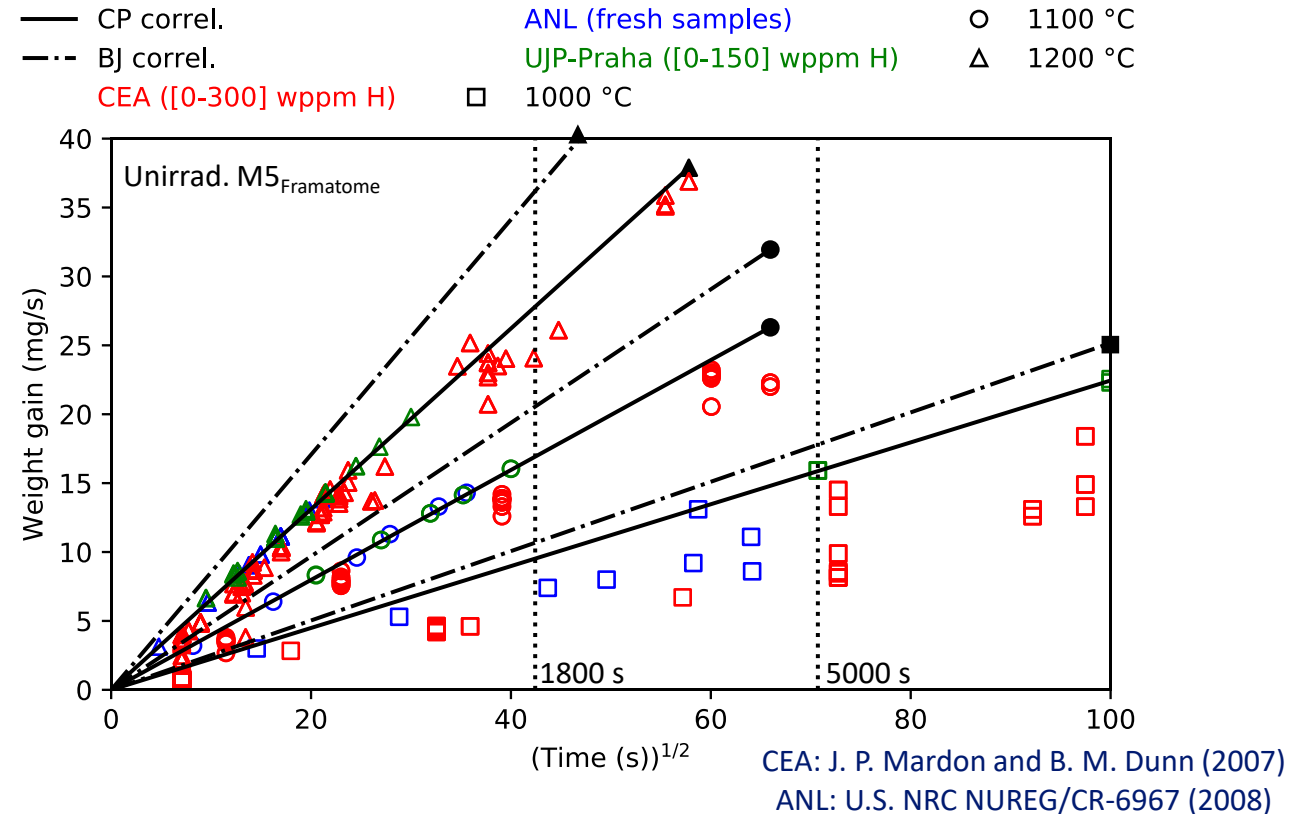
Shortest onset time typically occurs for $T \sim 1000^{\circ}\text{C}$

High-temperature oxidation kinetics

- No impact of irradiation on oxidation kinetic
- Cathcart-Pawel and Baker-Just correlations can be used up to 1204 °C



Adapted from figure 7 of M. Amaya et al. 2018



CEA: J. P. Mardon and B. M. Dunn (2007)

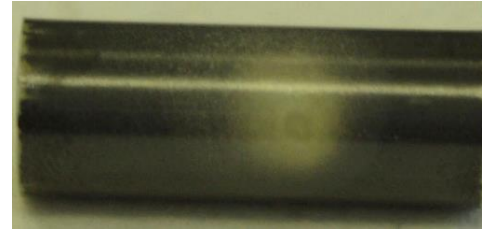
ANL: U.S. NRC NUREG/CR-6967 (2008)

Susceptibility to the breakaway oxidation phenomenon

- High resistance of M5_{Framatome} to breakaway oxidation, up to 15000 s at 1000 °C as already been demonstrated by CEA (M. Le Saux et al. 2020)
- Tests were performed at Framatome's Paimboeuf facility (V. Garat et al. 2016) on artificially scratched samples (S) (~50 µm depth and ~100 µm width)
- No discernible impact of scratches on M5_{Framatome} up to 10000 s at 1000 °C

ZIRLO

U.S. NRC NUREG/CR-6967 (2008)



Standard ZIRLO, 985 °C 3600 s
270±165 wppm H



Scratched ZIRLO, 985 °C 3400 s
155±98 wppm H

M5_{Framatome}

1000 °C 5000 s
19 wppm H

1000 °C 10000 s
36 wppm H

Standard



Scratched



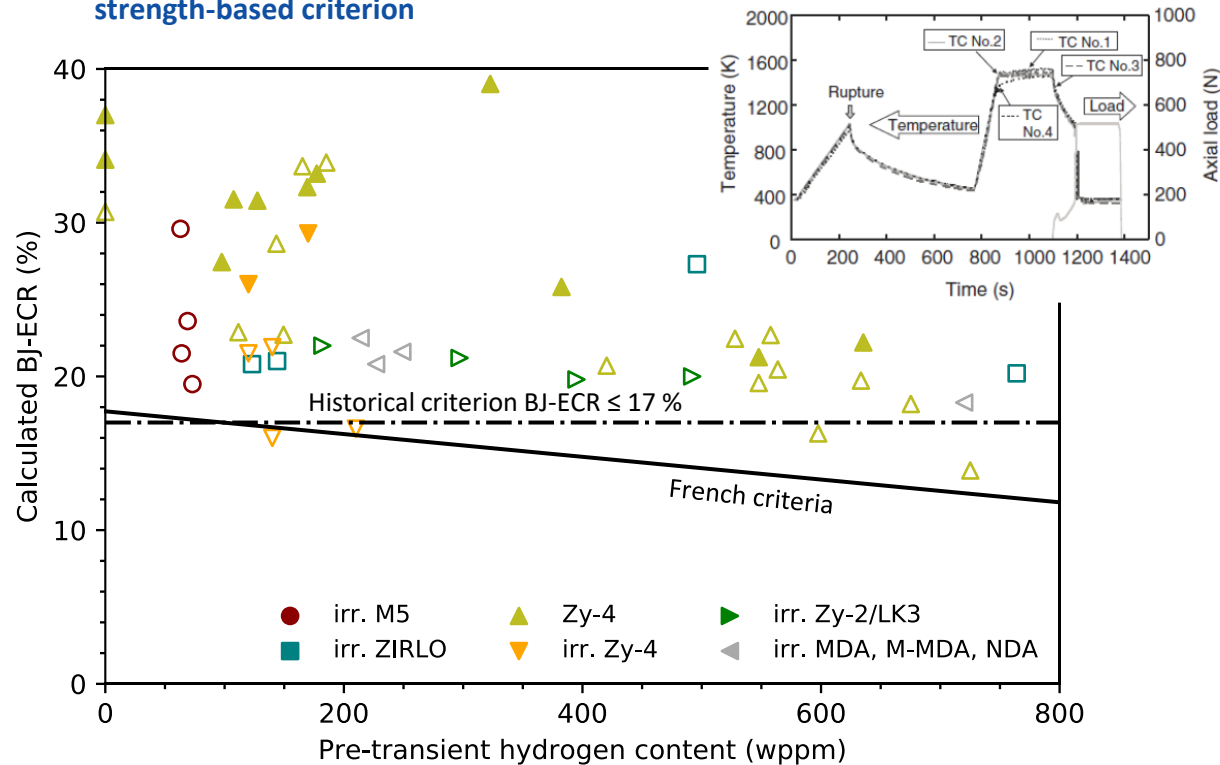
14 wppm H

13 wppm H

Post-oxidation mechanical behavior

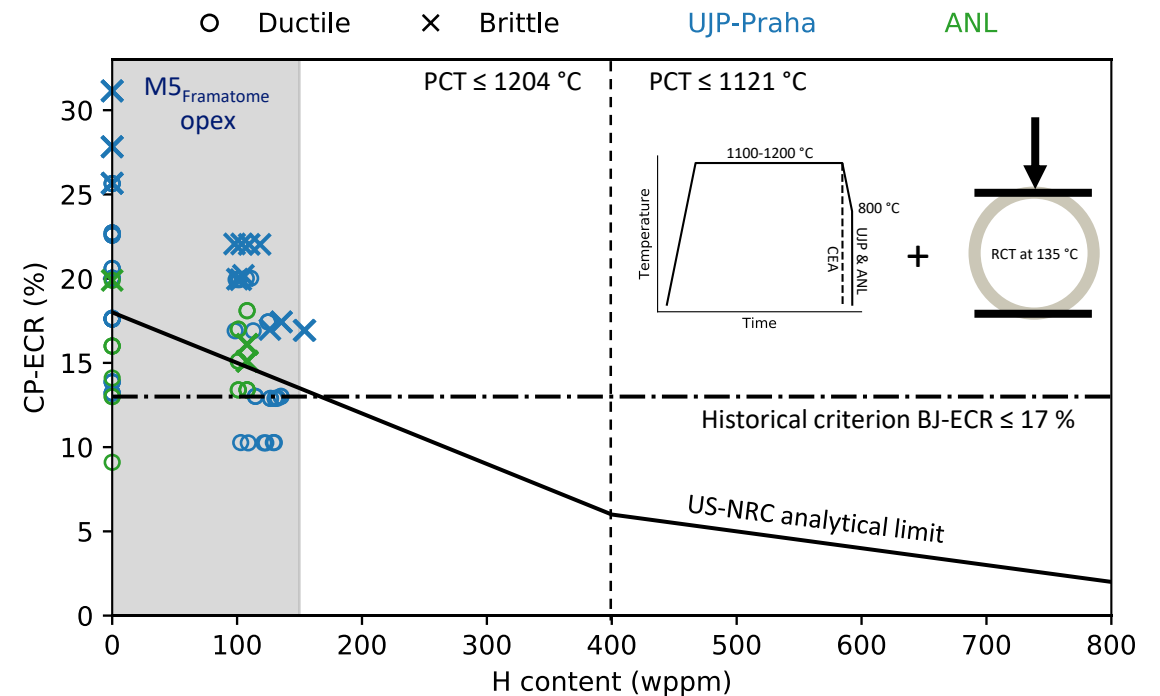
Embrittlement determined by axial loading during quench

- LOCA semi-integral testing performed by JAEA on fresh, pre-hydrated and irradiated (66-84 GWd/t) claddings*
- Axial loading ranged from 0 to 540 N
- **M5_{Framatome} maintains a high degree of margin with respect to the French strength-based criterion**



Post-quench ductility determined by RCT

- ANL (U.S. NRC NUREG/CR-6967 and DG-1262) and UJP-Praha: two-sided oxidation and quench from 800 °C
- **M5_{Framatome} maintains a high degree of margin with respect to the analytical limit proposed in draft DG-1263**



Conclusion

- LOCA regulatory framework has evolved as experimental data has allowed better understanding of the impacts of corrosion on safety margin and the role that the pre-transient hydrogen plays in coolability
- Extensive experimental testing on M5_{Framatome} cladding has demonstrated:
 - Low H uptake in nominal conditions, for both typical PWR and VVER environments
 - High-temperature oxidation kinetics well predicted by the CP and BJ correlations
 - Sufficient mechanical properties remain after high-temperature oxidation to retain a coolable geometry
 - M5_{Framatome} resistance to breakaway oxidation, even with scratches, assures it will not occur during a LOCA
- In conclusion, **M5_{Framatome} maintains a high degree of margin with respect to both the US and French H-dependent analytical limits for LOCA**

Acknowledgment:

Framatome thanks JAEA, CEA and UJP-Praha for their experimental work involving M5_{Framatome} cladding.

References

- U.S. NRC, Draft Regulatory Guide DG-1263 (2014)
Establishing analytical limits for zirconium based alloy cladding
- U.S. NRC, Draft Regulatory Guide DG-1262 (2014)
Testing for postquench ductility
- U.S. NRC, NUREG/CR-6967 (2008)
Cladding Embrittlement During Postulated Loss-of-Coolant Accidents
- Cabrera, A. and N. Waackel (2015)
“A Strength Based Approach to Define LOCA Limits”,
TopFuel 2015
- M. Le Saux et al. (2020)
Breakaway oxidation of zirconium alloys exposed to steam around 1000 °C
Corrosion science
- V. Garat et al. (2016)
AREVA NP M5® Cladding Benefits for Proposed US NRC RIA and LOCA
Requirements
TopFuel 2016
- M. AMAYA et al. (2018)
Behaviors of High-burnup LWR Fuels with Improved Materials under
Design-basis Accident Conditions
TopFuel 2018
- J. P. Mardon and B. M. Dunn (2007)
Overview of the M5® alloy behavior under RIA and LOCA conditions
Top Fuel 2007
- F. Nagase and T. Fuketa (2005)
Behavior of Pre-hydrated Zircaloy-4 Cladding under Simulated LOCA Conditions
Journal of Nuclear Science and Technology
- F. Nagase and T. Fuketa (2006)
Fracture Behavior of Irradiated Zircaloy-4 Cladding under Simulated LOCA Conditions
Journal of Nuclear Science and Technology
- F. Nagase, T. Chuto, and T. Fuketa (2009)
Behavior of High Burn-up Fuel Cladding under LOCA Conditions
Journal of Nuclear Science and Technology
- T. Narukawa and M. Amaya (2020)
Fracture limit of high-burnup advanced fuel cladding tubes under loss-of-coolant accident
conditions,”
Journal of Nuclear Science and Technology

Thank
you

Any reproduction, alteration, transmission to any third party or publication in whole or in part of this document and/or its content is prohibited unless Framatome has provided its prior and written consent.

This document and any information it contains shall not be used for any other purpose than the one for which they were provided.

Legal and disciplinary actions may be taken against any infringer and/or any person breaching the aforementioned obligations.